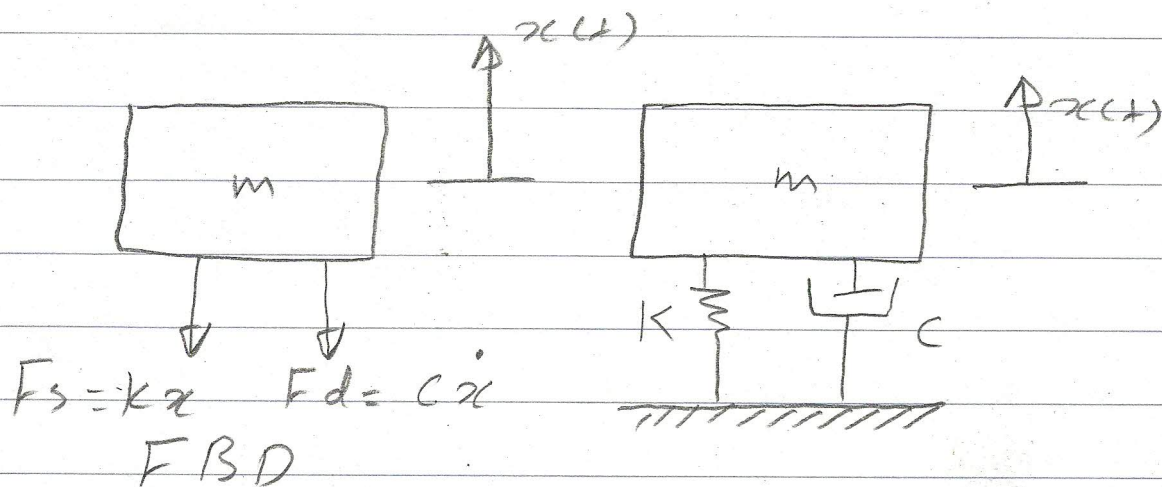


(1)

Free Vibration of damped system

For simple mass-spring-damper system



Applying Newton's second law $\sum F = m\ddot{x}$
 $-c\dot{x} - kx = m\ddot{x} \Rightarrow m\ddot{x} + c\dot{x} + kx = 0$
 $\ddot{x} + \frac{c}{m}\dot{x} + \frac{k}{m}x = 0$

Let $\frac{c}{m} = 2\zeta\omega_n$ $\frac{k}{m} = \omega_n^2$

$$\ddot{x} + 2\zeta\omega_n\dot{x} + \omega_n^2x = 0 \quad \text{--- (1)}$$

Where $\zeta = \frac{c}{2m\omega_n}$ is called Viscous damping factor

ζ is non-dimensional parameter

Solution $x(t) = A e^{st}$ where A, s are constants to be determined

$$\dot{x}(t) = A s e^{st} = s x(t) \text{ and } \ddot{x} = A s^2 e^{st}$$

$$\ddot{x} = s^2 x(t)$$

Substitute in Eq. (1)

$$s^2 x(t) + 2\zeta\omega_n s x(t) + \omega_n^2 x(t) = 0$$

$$s^2 + 2\zeta\omega_n s + \omega_n^2 = 0 \quad \text{--- (2)}$$

Equation (2) is called characteristic

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Equation of the system and it is a quadratic equation in S

$$S_{1,2} = \frac{-2\{\omega_n \mp \sqrt{4\omega_n^2 \zeta^2 - 4\omega_n^2}}{2}$$

$$S_{1,2} = \omega_n \left[-\zeta \pm \sqrt{\zeta^2 - 1} \right]$$

$$S_{1,2} = \omega_n \left[-\zeta \pm i\sqrt{1 - \zeta^2} \right]$$

The nature of the roots $S_{1,2}$ depends on the value of ζ

Discuss four values of ζ namely $\zeta = 0$, $\zeta = 1$, $0 < \zeta < 1$ and $\zeta > 1$

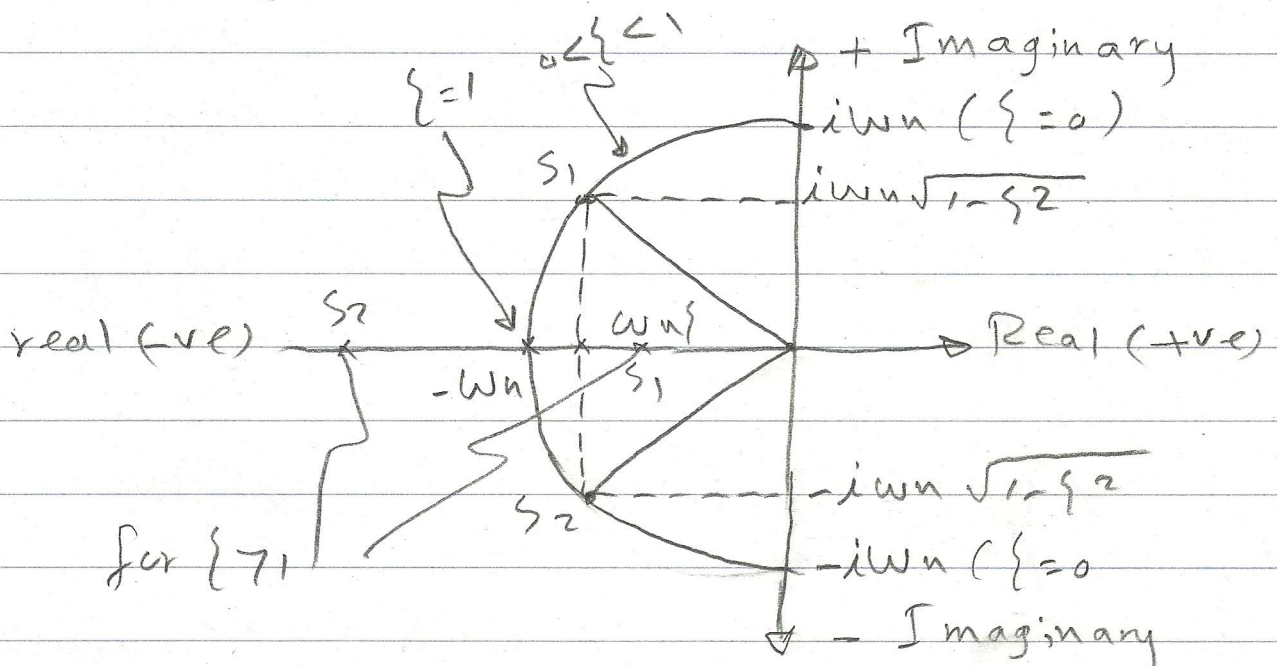
When $\zeta = 0$ $S_{1,2} = \pm i\omega_n$

When $0 < \zeta < 1$

$S_{1,2}$ are complex conjugates with respect to the real axis on a circle of radius ω_n

When $\zeta = 1$ $S_{1,2} = -\omega_n$

When $\zeta > 1$ $S_1 \rightarrow 0$ and $S_2 \rightarrow -\infty$



(2)

The solution will be $s_1 t$ $s_2 t$

$$x(t) = A_1 e^{s_1 t} + A_2 e^{s_2 t}$$

Case (a) underdamped case $0 < \zeta < 1$

$$-\zeta \omega_n t \pm i \omega_n t \sqrt{1-\zeta^2} \quad -\zeta \omega_n t \mp i \omega_n t \sqrt{1-\zeta^2}$$

$$x(t) = A_1 e^{s_1 t} + A_2 e^{s_2 t}$$

$$e^{-\zeta \omega_n t} e^{\pm i \omega_n t \sqrt{1-\zeta^2}} \quad e^{-\zeta \omega_n t} e^{\mp i \omega_n t \sqrt{1-\zeta^2}}$$

$$x(t) = e^{-\zeta \omega_n t} \left[A_1 e^{i \omega_d t} + A_2 e^{-i \omega_d t} \right]$$

Let $\omega_d = \omega_n \sqrt{1-\zeta^2}$, ω_d is called frequency of damped free vibration

$$x(t) = e^{-\zeta \omega_n t} \left[A_1 e^{i \omega_d t} + A_2 e^{-i \omega_d t} \right]$$

$$\text{but } e^{\pm i \omega_d t} = \cos \omega_d t \pm i \sin \omega_d t$$

$$\therefore x(t) = e^{-\zeta \omega_n t} \left[A_1 \cos \omega_d t + i A_1 \sin \omega_d t \right.$$

$$\left. + A_2 \cos \omega_d t - i A_2 \sin \omega_d t \right]$$

$$x(t) = e^{-\zeta \omega_n t} \left[\cos \omega_d t (A_1 + A_2) + i \sin \omega_d t (A_1 - A_2) \right]$$

$$\text{Let } A_1 + A_2 = A \cos \phi$$

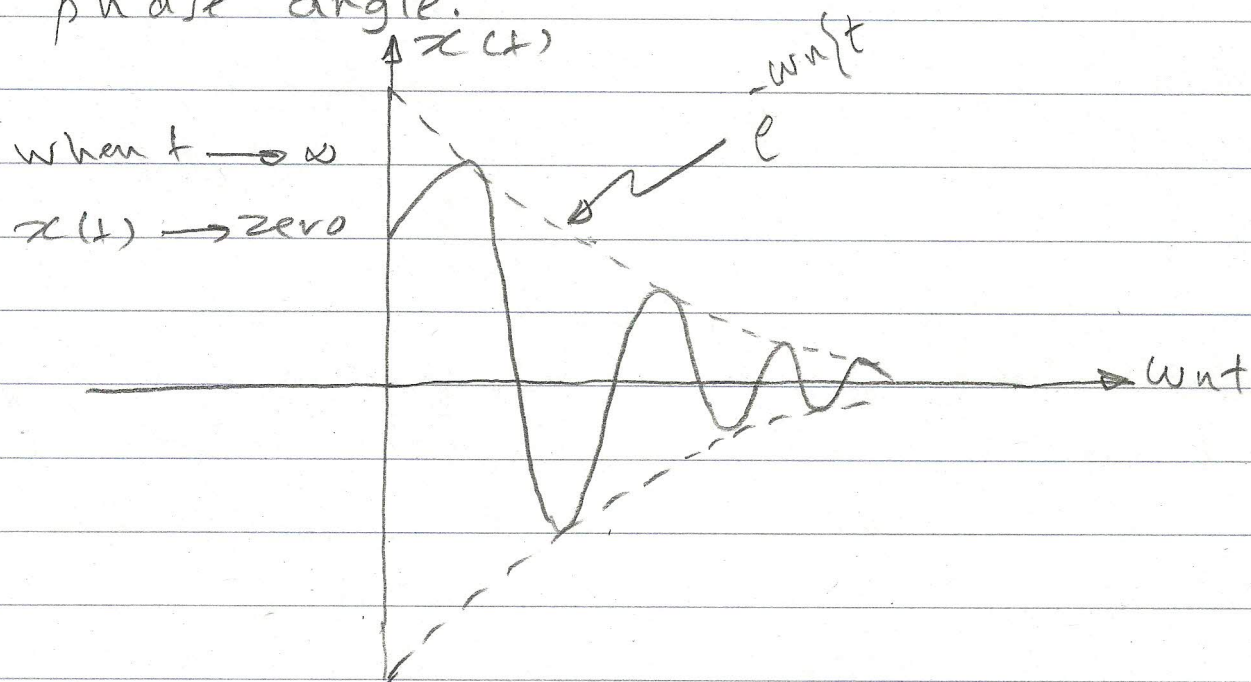
$$\text{and } i(A_1 - A_2) = A \sin \phi$$

$$x(t) = e^{-\zeta \omega_n t} \left[A \cos \phi \cos \omega_d t + A \sin \phi \sin \omega_d t \right]$$

$$x(t) = A e^{-\zeta \omega_n t} \cos(\omega_d t - \phi)$$

(2)

Where A , ϕ are constant depending on the initial condition $x(0)$, $\dot{x}(0)$ and they are called amplitude and phase angle.



Thus this case is called Oscillatory motion case.

Case (b) Overdamped case $\{\gamma > 1$

The roots

$s_{1,2} = \omega_n (-\{\pm \sqrt{\{\gamma^2 - 1\}})$ are always real roots

$s_1 \rightarrow \text{zero}$ and $s_2 \rightarrow -\infty$

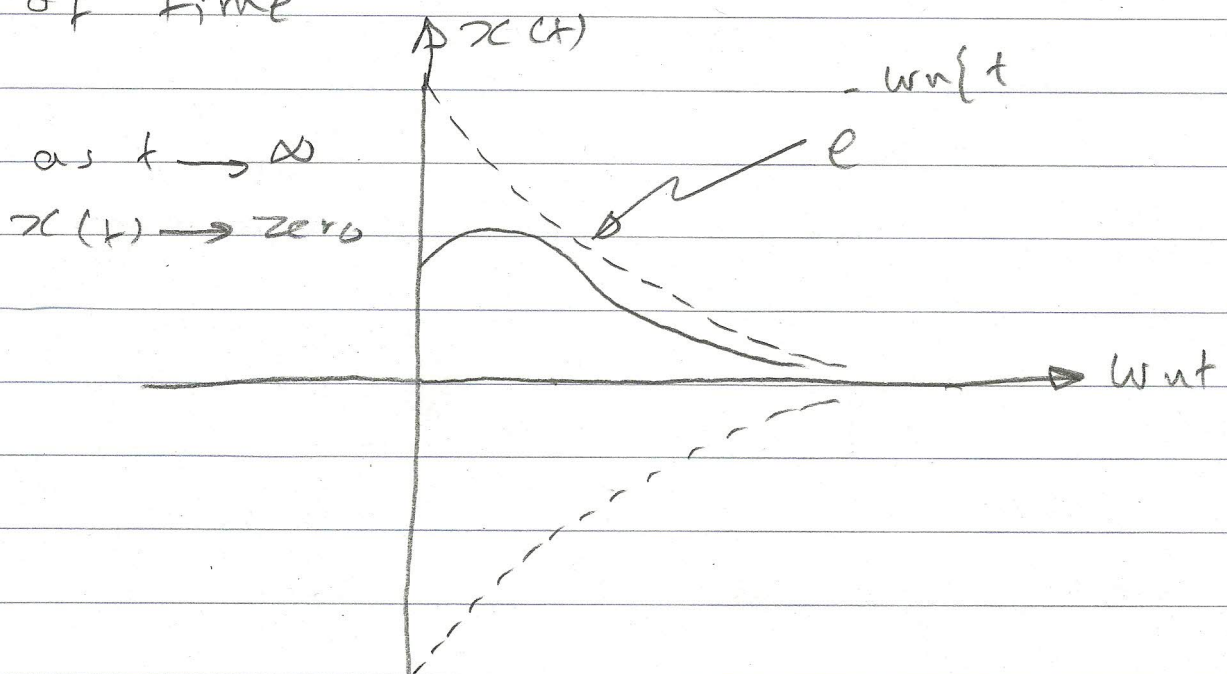
The general solution is

$$x(t) = e^{-\{\omega_n t\}} \left[A_1 e^{(\sqrt{\{\gamma^2 - 1\}} \omega_n t) - \omega_n t \sqrt{\{\gamma^2 - 1\}}} + A_2 e^{-\omega_n t \sqrt{\{\gamma^2 - 1\}}} \right]$$

So there is no imaginary roots, hence no harmonic motion and the motion

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is an exponentially decreasing function of time



So this case is called non-oscillatory motion case.

Case (c) Critical damping $\zeta = 1$

$$\frac{c}{m} = 2\omega_n \quad \text{when } \zeta = 1 \quad c = c_{cr}$$

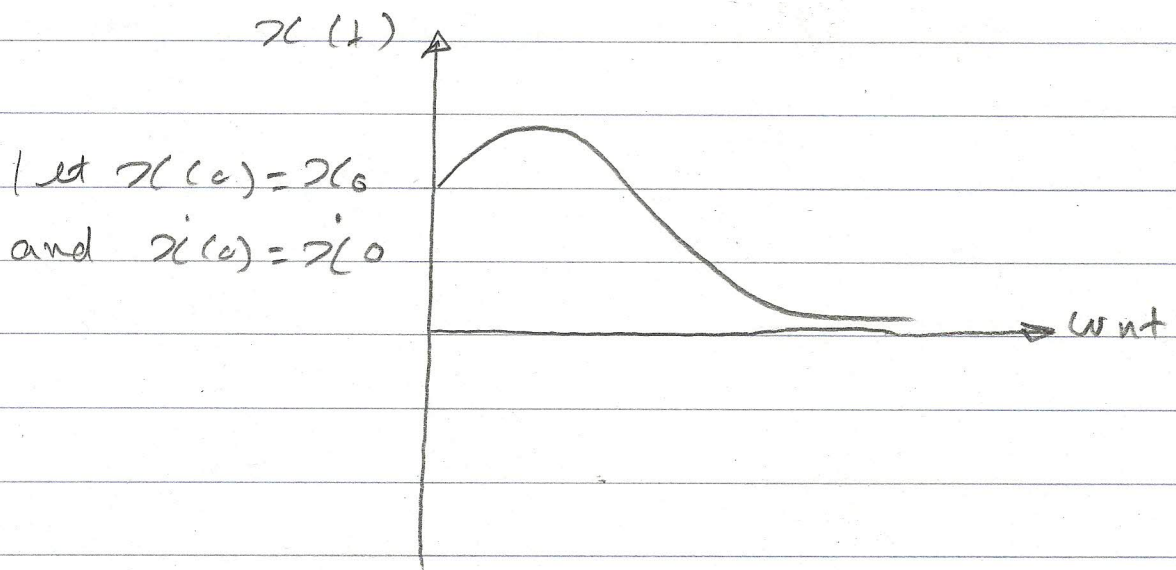
$$c_{cr} = 2m\omega_n \quad \text{but } \omega_n = \sqrt{\frac{k}{m}}$$

$$c_{cr} = 2m\sqrt{\frac{k}{m}} = 2\sqrt{\frac{m^2 k}{m}} = 2\sqrt{mk}$$

It is not important case because it is the borderline between the oscillatory and non-oscillatory cases.

The roots $s_{1,2} = -\omega_n$ and the solution is $x(t) = (A_1 + tA_2)e^{-\omega_n t}$

(5)



$A_1 = x_0$ and $A_2 = x'_0 + x_0 \omega_n$
 \therefore The solution will be

$$x(t) = [x_0 + (x'_0 + x_0 \omega_n)t] e^{-\omega_n t}$$

Case (d) undamped case $\zeta = 0$
 which is discussed previously in
 vibration of undamped system
 Solution

$$x(t) = A \cos(\omega_n t - \phi)$$

Example 1: For a simple spring-mass-damper system, the initial conditions are $x(0) = 0$ and $x'(0) = V_0$. Calculate the response for $\zeta > 1$, $\zeta = 1$ and $0 < \zeta < 1$.

① For $\zeta > 1$

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$$x(t) = e^{-\{\omega_n t\}} \left[A_1 e^{\omega_n t \sqrt{\xi^2 - 1}} + A_2 e^{-\omega_n t \sqrt{\xi^2 - 1}} \right]$$

$$\text{at } t=0 \quad x(0) = A_1 + A_2 = 0 \rightarrow A_1 = -A_2$$

$$x(t) = e^{-\{\omega_n t\}} \left[A_1 e^{\omega_n t \sqrt{\xi^2 - 1}} - A_1 e^{-\omega_n t \sqrt{\xi^2 - 1}} \right] \times \frac{2}{2}$$

$$\therefore x(t) = 2 A_1 e^{-\{\omega_n t\}} \sinh \omega_n t \sqrt{\xi^2 - 1}$$

$$\dot{x}(t) = 2 A_1 (-\{\omega_n\}) e^{-\{\omega_n t\}} \sinh \omega_n t \sqrt{\xi^2 - 1}$$

$$+ 2 A_1 e^{-\{\omega_n t\}} (\omega_n \sqrt{\xi^2 - 1}) \cosh \omega_n t \sqrt{\xi^2 - 1}$$

$$\dot{x}(t) = 2 A_1 \omega_n \left[\sqrt{\xi^2 - 1} \cosh \omega_n t \sqrt{\xi^2 - 1} - \sinh \omega_n t \sqrt{\xi^2 - 1} \right]$$

$$\text{at } t=0 \quad \dot{x}(0) = 2 A_1 \omega_n \sqrt{\xi^2 - 1} = V_0$$

$$\therefore A_1 = \frac{V_0}{2 \omega_n \sqrt{\xi^2 - 1}} = -A_2$$

\therefore The solution (Response) will be

$$x(t) = \frac{V_0}{\omega_n \sqrt{\xi^2 - 1}} e^{-\{\omega_n t\}} \sinh \omega_n t \sqrt{\xi^2 - 1}$$

(4)

$$\text{For } \zeta = 1 \quad x(t) = (A_1 + tA_2)e^{-\omega_n t}$$

$$\text{at } t=0 \quad x(0)=0 \rightarrow A_1=0$$

$$\dot{x}(t) = tA_2(-\omega_n)e^{-\omega_n t} + A_2e^{-\omega_n t}$$

$$\dot{x}(t) = A_2 \left[e^{-\omega_n t} - t\omega_n e^{-\omega_n t} \right]$$

$$\dot{x}(t) = e^{-\omega_n t} A_2 (1 - t\omega_n)$$

$$\text{at } t=0 \quad \dot{x}(0)=V_0 \rightarrow V_0 = A_2$$

\therefore The solution (Response) will be

$$x(t) = V_0 t e^{-\omega_n t}$$

$$\text{For } 0 < \zeta < 1 \quad x(t) = Ae^{-\zeta\omega_n t} \cos(\omega_d t - \phi)$$

$$\text{at } t=0 \quad x(0)=0 \rightarrow 0 = A \cos(-\phi)$$

$$A \neq 0 \quad \therefore \cos -\phi = 0 \rightarrow \phi = \frac{\pi}{2}$$

$$x(t) = Ae^{-\zeta\omega_n t} \cos(\omega_d t - \frac{\pi}{2}) = Ae^{-\zeta\omega_n t} \sin \omega_d t$$

$$\dot{x}(t) = A \left[\omega_d e^{-\zeta\omega_n t} \cos \omega_d t - \omega_n e^{-\zeta\omega_n t} \sin \omega_d t \right]$$

$$\text{at } t=0 \quad \dot{x}(0)=V_0 \rightarrow V_0 = A \omega_d \rightarrow A = \frac{V_0}{\omega_d}$$

\therefore The solution (Response) will be

$$x(t) = \frac{V_0}{\omega_d} e^{-\zeta\omega_n t} \sin \omega_d t$$

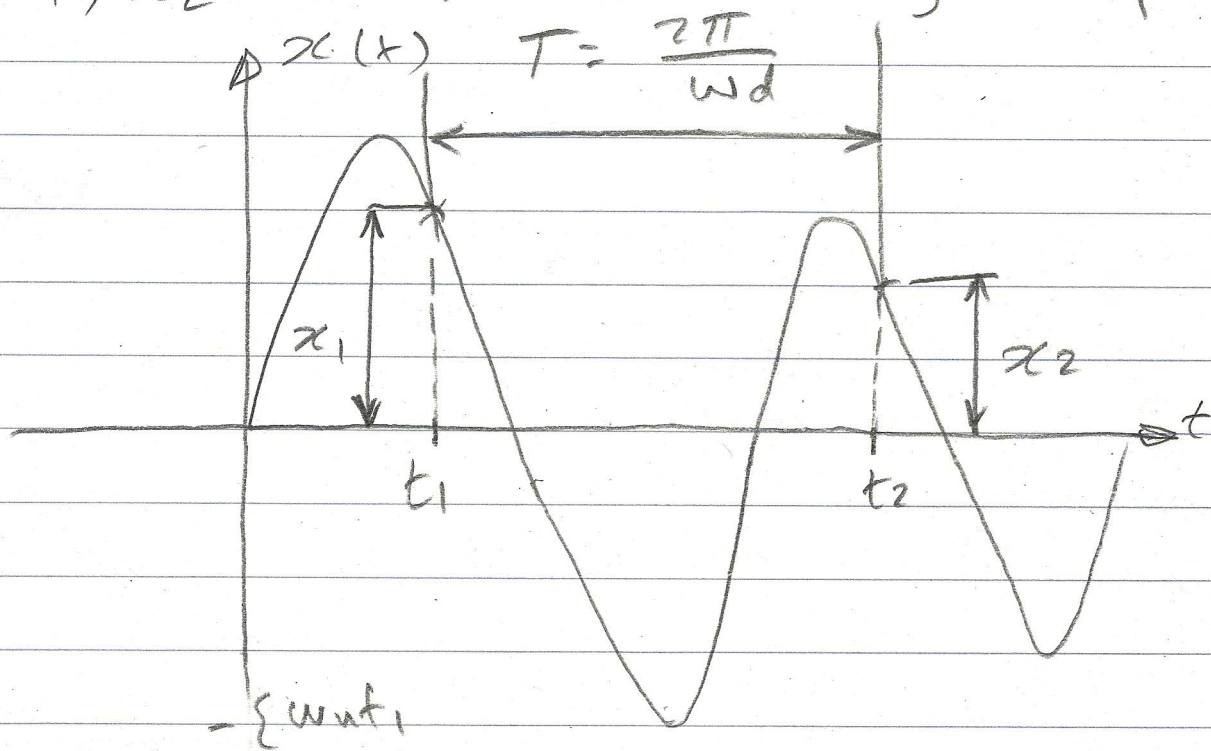
$$\text{where } \omega_d = \omega_n \sqrt{1 - \zeta^2}$$

(5)

Logarithmic Decrement

In case of underdamped free vibration, viscous damping causes the vibration to decay exponentially, so δ can be determined from the observation of this decay.

Let t_1, t_2 the time corresponding to two consecutive displacements x_1, x_2 measured one cycle apart.



$$x_1 = A e^{-\delta \omega_n t_1} \cos(\omega_d t_1 - \phi)$$

$$x_2 = A e^{-\delta \omega_n t_2} \cos(\omega_d t_2 - \phi)$$

$$\frac{x_1}{x_2} = \frac{A e^{-\delta \omega_n t_1} \cos(\omega_d t_1 - \phi)}{A e^{-\delta \omega_n t_2} \cos(\omega_d t_2 - \phi)}$$

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$$\text{but } t_2 = t_1 + T, T = \frac{2\pi}{\omega_d}$$

$$\therefore \cos(\omega_d t_1 - \phi) = \cos(\omega_d t_2 - \phi)$$

$$\therefore \frac{x_1}{x_2} = \frac{e^{-\{\omega_n t_1\}}}{e^{-\{\omega_n(t_1+T)\}}} = e^{\{\omega_n T\}}$$

Let δ - logarithmic decrement

$$\delta = \ln \frac{x_1}{x_2}$$

$$\text{So } \ln \frac{x_1}{x_2} = \delta = \{\omega_n T\} = \left\{ \omega_n + \frac{2\pi}{\omega_d} \right\}$$

$$\omega_d = \omega_n \sqrt{1 - \zeta^2}$$

$$\delta = \zeta \times \frac{2\pi}{\sqrt{1 - \zeta^2}}$$

$$\delta \sqrt{1 - \zeta^2} = 2\pi \zeta \rightarrow \delta^2 (1 - \zeta^2) = (2\pi \zeta)^2$$

$$\zeta^2 ((2\pi)^2 + \delta^2) = \delta^2 \rightarrow \zeta = \frac{\delta}{\sqrt{(2\pi)^2 + \delta^2}}$$

For small damping δ is small quantity

$$\therefore \zeta = \frac{\delta}{2\pi}$$

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The Viscous damping factor ζ can also be determined by measuring two displacements separated by any number of complete cycles (j).

Let x_1 and x_{j+1} be the amplitudes corresponding to times t_1 and t_{j+1} and $t_{j+1} = t_1 + jT$, one can conclude that

$$\frac{x_1}{x_{j+1}} = \frac{x_1}{x_2} \cdot \frac{x_2}{x_3} \cdot \frac{x_3}{x_4} \cdots \frac{x_j}{x_{j+1}}$$

Because the ratio between any two consecutive displacements, one cycle apart is equal to $e^{\zeta \omega_n T}$

$$\therefore \ln \frac{x_1}{x_{j+1}} = j \zeta \omega_n T \quad \text{but } \zeta \omega_n T = \delta$$

$$\boxed{\ln \frac{x_1}{x_{j+1}} = j \delta} \rightarrow \boxed{\delta = \frac{1}{j} \ln \frac{x_1}{x_{j+1}}}$$

Ex 1 :: It was observed that the vibration amplitude of a damped single degree of freedom system has fallen by 50 per cent after five complete cycles. Calculate the viscous damping factor.

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$$\delta = \frac{1}{j} \ln \frac{x_1}{x_{j+1}} \quad j=5 \quad \delta = \frac{1}{5} \ln \frac{x_1}{x_6}$$

$$\frac{x_1}{x_6} = \frac{1}{0.5} \rightarrow x_6 = 0.5 x_1$$

$$\delta = \frac{1}{5} \ln \frac{x_1}{0.5 x_1} = \frac{1}{5} \ln 2 = 0.13863 \quad (\text{Small damping})$$

$$\therefore \left\{ \approx \frac{\delta}{2\pi} \right\} \rightarrow \left\{ \approx \frac{0.13863}{2\pi} \right\}$$

$$\left\{ = 0.02206 \right.$$

EX2: For small damping show that the logarithmic decrement can be expressed in terms of the vibrational energy U and the energy dissipated per cycle ΔU .

$$\delta = \ln \frac{x_1}{x_2} \rightarrow \frac{x_2}{x_1} = e^{-\delta} = 1 - \delta + \frac{\delta^2}{2!} - \frac{\delta^3}{3!} + \frac{\delta^4}{4!} - \frac{\delta^5}{5!} + \dots$$

The vibrational energy of a system is that stored in the spring at maximum displacement.

$$U_1 = \frac{1}{2} k x_1^2 = U \quad U_2 = \frac{1}{2} k x_2^2$$

$$\frac{\Delta U}{U} = \frac{U_1 - U_2}{U_1} = 1 - \frac{U_2}{U_1} = 1 - \left(\frac{x_2}{x_1} \right)^2 = 1 - e^{-2\delta}$$

$$\frac{\Delta U}{U} = 1 - \left(1 - 2\delta + \frac{(2\delta)^2}{2!} - \frac{(2\delta)^3}{3!} + \dots \right)$$

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$$\frac{DU}{U} = \sqrt{-1+2\delta} - \frac{(2\delta)^2}{2!} + \frac{(2\delta)^3}{3!} - \dots$$

For small damping $\delta^2 \approx 0$

$$\therefore \boxed{\frac{DU}{U} = 2\delta}$$